

Monte Carlo Methods in Iterative Solvers

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1st Workshop on Nonlinear Analysis of Shell Structures

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TASKS

- Development of new tools for reliability analysis
- Reducing computation cost of sensitivity analysis



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MAIN ACTIVITIES

- Development of numerical methods for Monte Carlo based sensitivity analysis in combination with FE-analysis
- Implementation of Monte Carlo simulation methods in combination with iterative methods
- Investigation of sensitivity with respect to input variables

APPROACH

- Generation of input sample with certain distributions (i.e. uniform distributions)
- Calculation of the model response for each of these input values
- Inspection of the distribution of output data (and its correlation to the input data)

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CHALLENGES

- Relies on multiple model calls
- Expensive computational cost if the model itself requires costly computations

IDEA

- Small changes in input parameters result in neighbouring equations
- Use data extracted from previous calculation for a speed up

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APPROACHES TO USE DATA FROM PREVIOUS SOLUTIONS

- iterative scheme
- preconditioned conjugated gradients (pcg)

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- Use a previously calculated solution as the starting vector

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PERFORMANCE (COMPUTATION TIME)

preconditioner	DOF	$spr = 1\%$	$spr = 5\%$	$spr = 10\%$
IC with $tol=1e-2$	5642	0.6570	0.6727	0.6919
cond with cholesky neighbour	5642	0.1167	0.1551	0.1615

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- Start parameter variation at a later step in the calculation

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APPROACH

- Start the FE computation using the nominal parameter values
- At some step n_{var} , change the input parameters and perform additional equilibrium iterations
- Continue with applying load steps until the target load is reached

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DIFFICULTIES

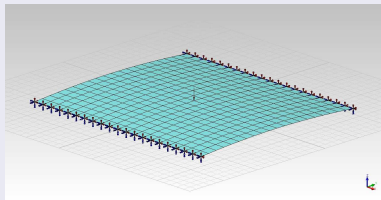
- Numerical solution of the problem may be path dependent
- Speed of convergence can be affected

MODEL: SHALLOW CYLINDRICAL ROOF

MODEL

Model input: F, E, ν

Model output: displacement in middle node

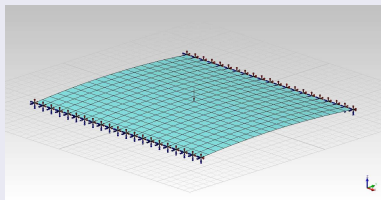


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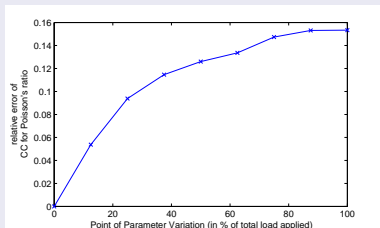
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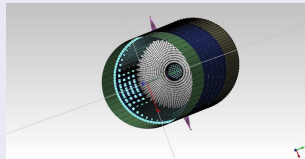
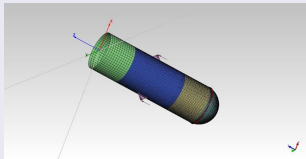
RESULT

- Correlation indicators change
- Ranking of indicators stays the same
- Significantly faster computation



SIMPLIFIED LAUNCHER MODEL

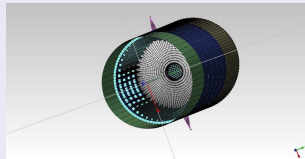
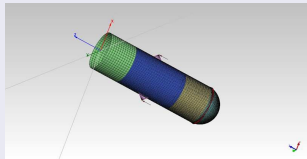
INPUT VARIABLES



Description of input parameters		
i	Parameter X_i	Mean μ_i
1	hydrostatic pressure cylinder3	0.4 MPa
2	hydrostatic pressure sphere1	0.4 MPa
3	hydrostatic pressure sphere2	0.4 MPa
4	aerodynamic pressure	-0.05 MPa
5	booster loads y-direction node1	40000 N
6	booster loads y-direction node2	20000 N
7	booster loads z-direction node1	3.e6 N
8	booster loads z-direction node2	1.e6 N
9	mechanical loads x-direction	100 N
10	mechanical loads y-direction	50 N
11	mechanical loads z-direction	300 N
Output: Load Proportionality Factor (LPF)		

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INPUT:

Uniform distributions with spread $\pm 15\%$ of nominal value

RESULTS

- Correlation indicators change in dependence of the point of parameter variation
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COMPUTATION COST

Point of parameter variation [as fraction of target load]	processing time [in 10^6 s]
0	5.801
0.5	3.947
1.0	3.587

SENSITIVITIES

<i>i</i>	Variation at beginning (load factor = 0.0)				Variation at load factor = 1.0			
	CC	SRC	RCC	SRCC	CC	SRC	RCC	SRCC
1	0.1113	0.1608	0.0556	0.2873	-0.0363	-0.0049	-0.0226	0.2252
2	-0.0102	0.1114	-0.0075	0.2550	-0.1187	-0.0158	-0.0902	0.1762
3	0.1207	0.1658	0.1083	0.2469	-0.0547	0.0083	-0.0406	0.1249
4	0.0011	0.0418	0.0526	0.2442	-0.0368	-0.0037	-0.0030	0.2086
5	-0.0548	-0.0021	-0.0737	0.1249	-0.0709	-0.0126	-0.0632	0.1733
6	-0.0664	-0.0566	-0.0932	0.0381	-0.0373	0.0061	-0.0436	0.1517
7	-0.9582	-0.9841	-0.9624	-0.8221	-0.9972	-0.9958	-0.9999	-0.8268
8	-0.0344	-0.0400	-0.0436	0.0683	-0.0055	0.0129	0.0030	0.1385
9	0.0112	0.0084	0.0647	0.2252	0.0124	-0.0132	0.0165	0.1764
10	0.0032	-0.0017	0.0150	0.1737	-0.0221	-0.0281	0.0015	0.1840
11	-0.0176	-0.0550	-0.0406	0.1025	-0.0002	0.0020	0.0045	0.2037

LIMITATIONS

- Evaluation of smaller sensitivities is difficult due to errors
- Model evaluation for frontskirt model still time intensive

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FUTURE POSSIBILITIES

- Further development of the presented algorithms
- Embedding algorithms into FE framework