

Stochastic Fourier Integral Operators for Parameter Estimation and Damage detection.

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IT Workshop 2018

Natters, October 18, 2018

October 18, 2018

The (3×3) -system of linear, homogeneous, isotropic elasticity:

$$\partial_t^2 \mathbf{u} = \frac{\mu}{\rho} \Delta \mathbf{u} + \frac{\lambda + \mu}{\rho} \nabla \times \nabla \mathbf{u} + \mathbf{f}$$

for the displacement $\mathbf{u}(\mathbf{x}, t)$ with the density ρ and the Lamé constants λ, μ .

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Focus on full space problem with acting body force $\mathbf{f}(\mathbf{x}, t)$. As initial state we assume $\mathbf{u}(\mathbf{x}, 0) = \mathbf{0}$ and $\mathbf{u}_t(\mathbf{x}, 0) = \mathbf{0}$.

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LAMÉ REPRESENTATION (1)

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There exist unique potentials Φ , Ψ such that

$$\mathbf{u} = \nabla \Phi + \nabla \times \Psi, \quad \nabla \cdot \Psi = 0$$

The potentials satisfy a system of decoupled wave equations

$$\partial_{tt} \Phi - c_l^2 \Delta \Phi = \varphi, \quad \partial_{tt} \Psi_j - c_s^2 \Delta \Psi_j = \psi_j, \quad j = 1, 2, 3$$

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with the lateral and transversal wave speeds given by

$$c_l^2 = \frac{\lambda + 2\mu}{\rho}, \quad c_s^2 = \frac{\mu}{\rho}$$

The scalar wave equation

$$\partial_t^2 u - c^2 \Delta u = f, \quad u|_{t=0} = \partial_t u|_{t=0} = 0$$

is transformed to a (decoupled) first order system of pseudodifferential operators by setting $u_{\pm} = (\partial_t \pm ic\sqrt{-\Delta})u$, resulting in

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The solution is given by the FIO representation

$$u_{\pm}(x, t) = \int_{\mathbb{R}^3} \int_0^t e^{i(x\xi \pm c|\xi|(t-s))} \widehat{f}(\xi, s) ds d\xi$$

and finally

$$u(x, t) = \frac{1}{2} \int_0^t (u_+(x, s) + u_-(x, s)) ds$$

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- Sensors measure time dependent signal (i.e. amplitude)
- Fourier integral operator solution in signal location.
- Calibrate Lamé parameters s.t. L_2 -difference of signals is minimized.

Let

$$\begin{cases} \partial_{tt} \mathbf{u} = \frac{1}{\rho} \mu \Delta \mathbf{u} + (\lambda + \mu) \nabla(\nabla \cdot \mathbf{u}) + \mathbf{f} \\ \mathbf{u}|_{t=0} = 0 \\ \partial_t \mathbf{u}|_{t=0} = 0 \end{cases}$$

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Furthermore, $\tilde{\delta}$ is a smooth approximation to the delta distribution
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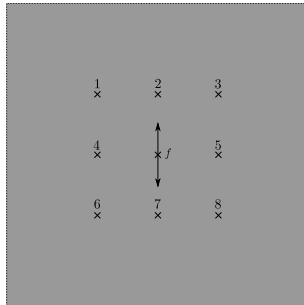
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We assume sensors around the center give time dependent signal
i.e. $h_i(t) := u(x_i, y_i, z_i, t), i = 1 \dots 8$

Using FIOs for parameter estimation:

- Measurement is represented with FEM-signal $f_{FEM}(t)$ in sensor location with unknown (E_{FEM}, ν_{FEM}) .
 - 256×256 elements (approx 15 min).
 - Abaqus, implicit time integration.



Using FIOs for parameter estimation:

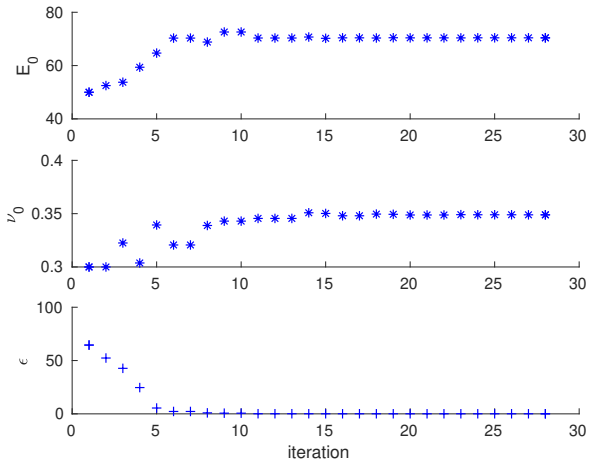
- Measurement is represented with FEM-signal $f_{FEM}(t)$ in sensor location with unknown (E_{FEM}, ν_{FEM}) .
- FIO-solution $f_{FIO}(t)$ in sensor location with known (E_{FEM}, ν_{FEM}) .
 - 256×256 grid.
 - 3 seconds to evaluate.

Using FIOs for parameter estimation:

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- FIO-solution $f_{FIO}(t)$ in sensor location with known (E_{FEM}, ν_{FEM}) .
- Minimize

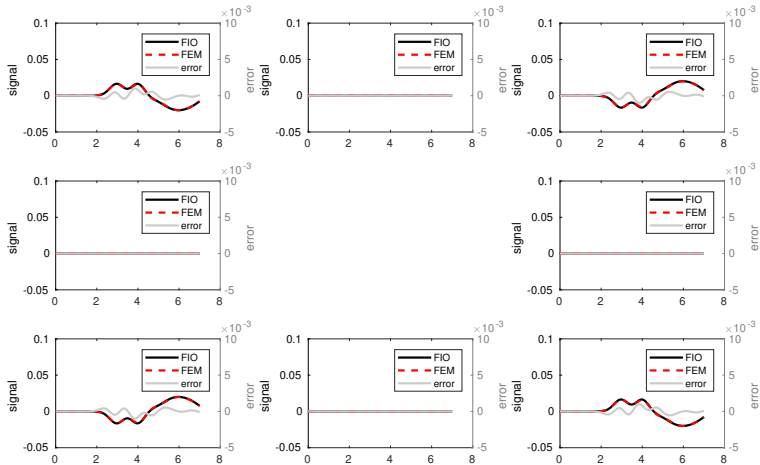
$$\|f_{FEM} - f_{FIO}(\cdot, E_{FIO}, \nu_{FIO})\|_{L_2}.$$

2D EXAMPLE

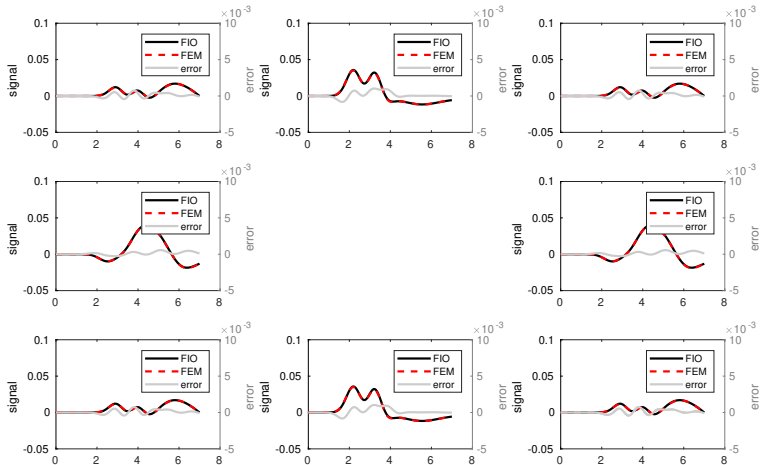


	Youngs Modulus	Poisson ratio
FEM	70.00 GPa	0.3500
optimized	70.41 GPa	0.3489

2D EXAMPLE

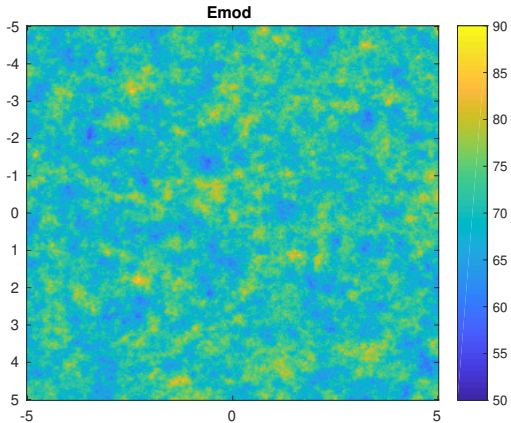


2D EXAMPLE



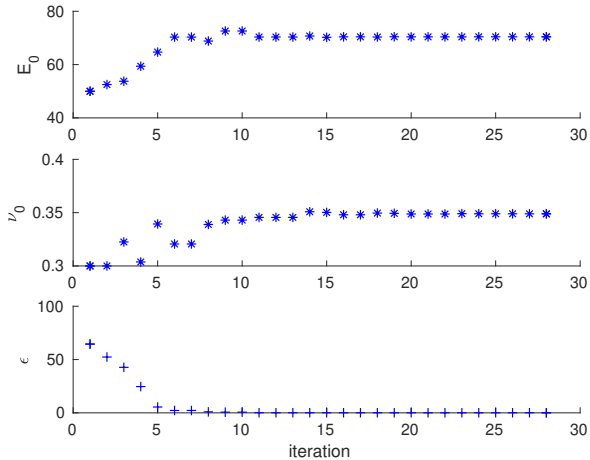
What if Lamé parameters are not
"clean"?

2D EXAMPLE



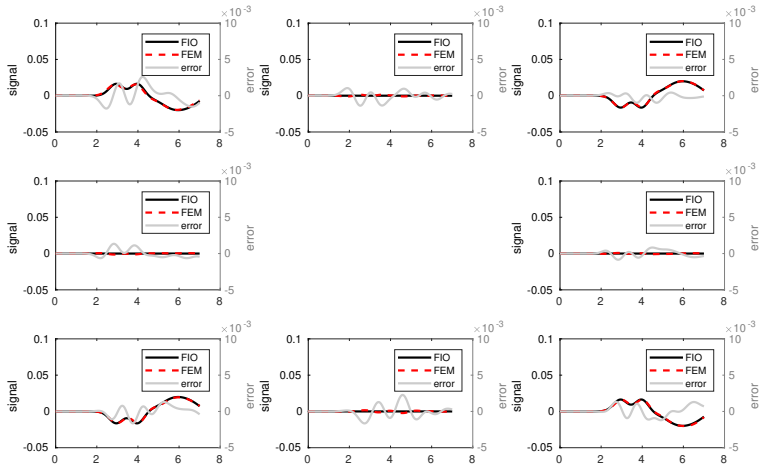
Perturbed random field in FEM Model (5% deviation).

2D EXAMPLE

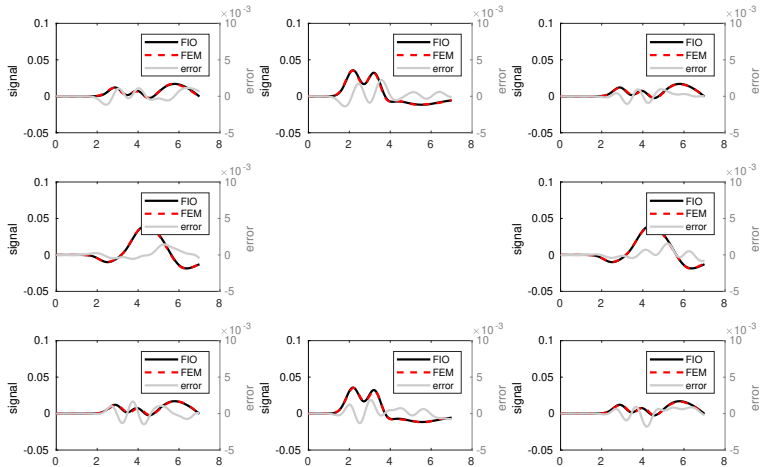


	Youngs Modulus	Poisson ratio
FEM nominal value	70.00 GPa	0.3500
optimized	70.97 GPa	0.3510

2D EXAMPLE



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Also possible:

- Variance estimation of FEM random field:
Compare variance of estimated parameters with variance of random field.

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Compare correlation of estimated parameters with correlation length of random field.

*with some limitations

- The usual FIO is of form:

$$\int e^{ix \cdot \xi \pm ic \|\xi\| t} \widehat{u}(\xi) \, d\xi$$

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- Add random perturbations:

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- Generate Monte Carlo sample and test if measurement differs too much from sample.

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- Random perturbation of FIO 5% of nominal value. Using random field.

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$$\int e^{ix \cdot y \pm c \|\xi\|^t} \widehat{u}(\xi) d\xi$$

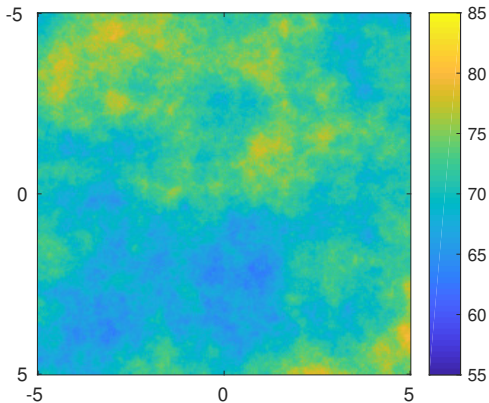
becomes

$$\int e^{ix \cdot y \pm c_\omega(x) \|\xi\|^t} \widehat{u}(\xi) d\xi.$$

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- Select features of signal:
 - Phase angle of dominant frequencies
 - Amplitude of dominant frequencies

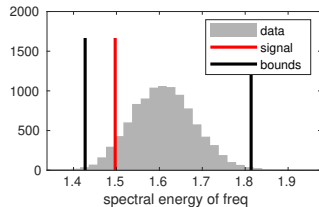
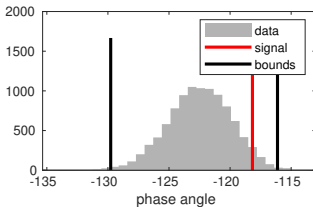
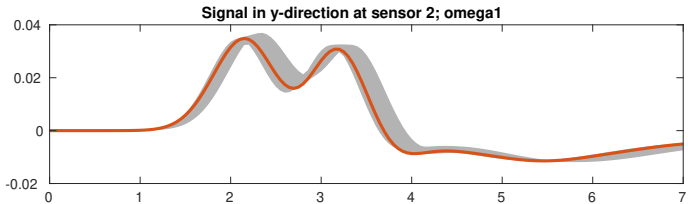
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- Select features of signal:
 - Phase angle of dominant frequencies
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- 4 scenarios:
 - 1 Material ok
 - 2 Youngs modulus too small
 - 3 Youngs modulus too large
 - 4 Crack (set Young's modulus to zero)

2D EXAMPLE

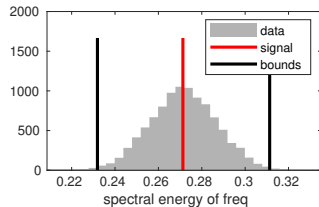
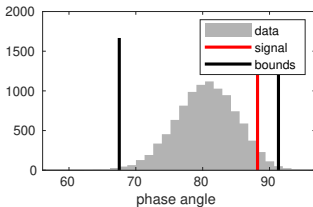
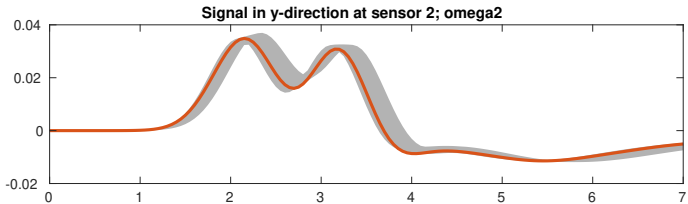


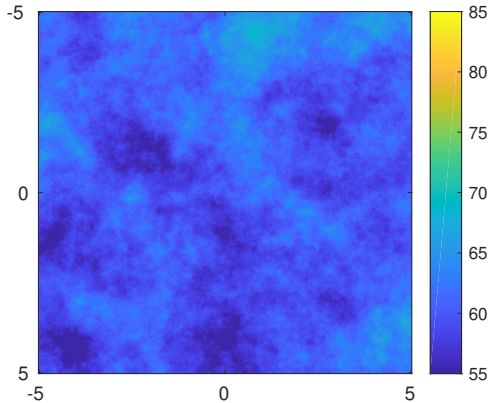
Material "ok"

2D EXAMPLE



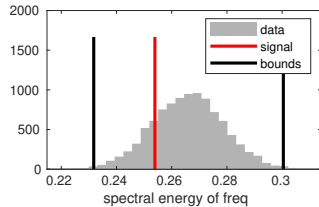
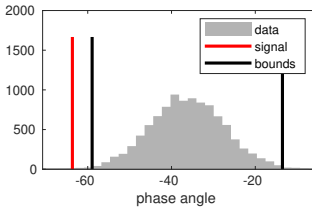
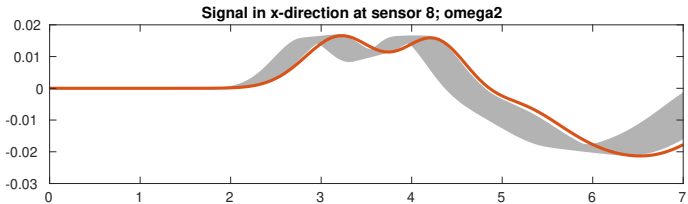
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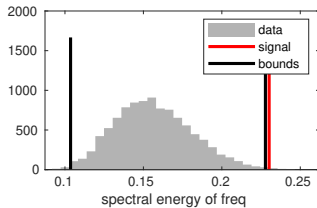
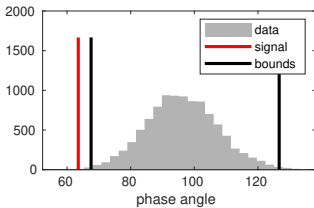
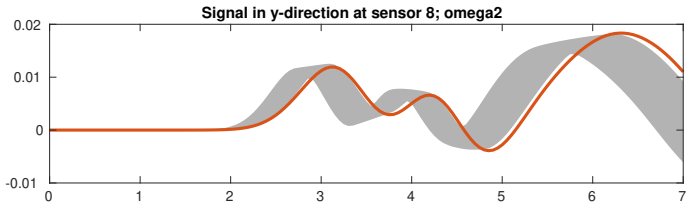


Young's modulus too small

2D EXAMPLE

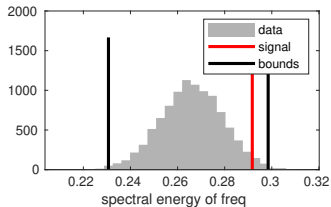
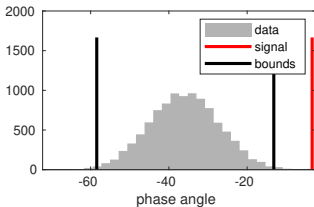
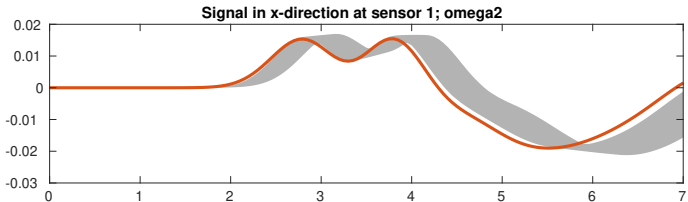


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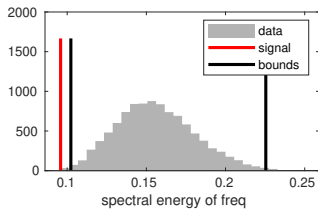
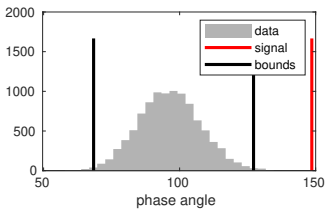
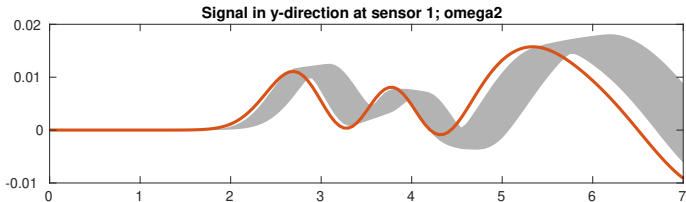


Young's modulus too large

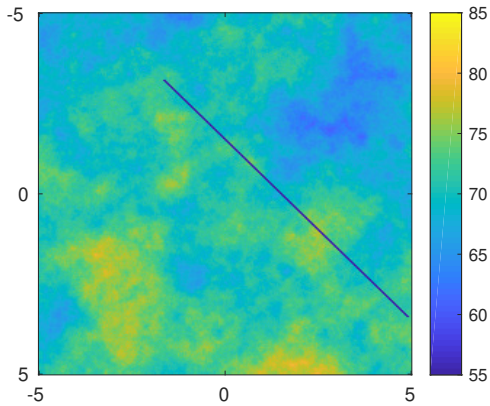
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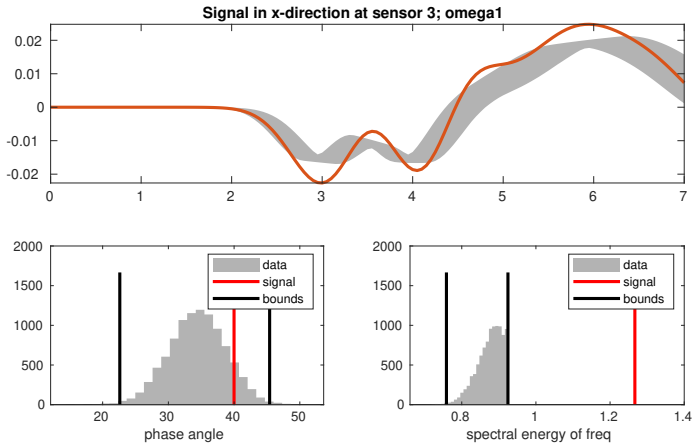


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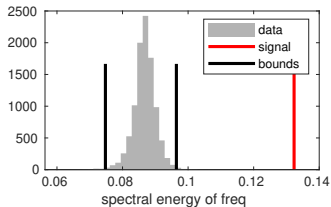
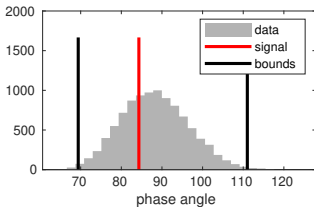
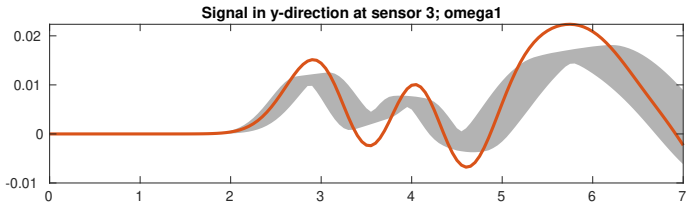


Crack

2D EXAMPLE



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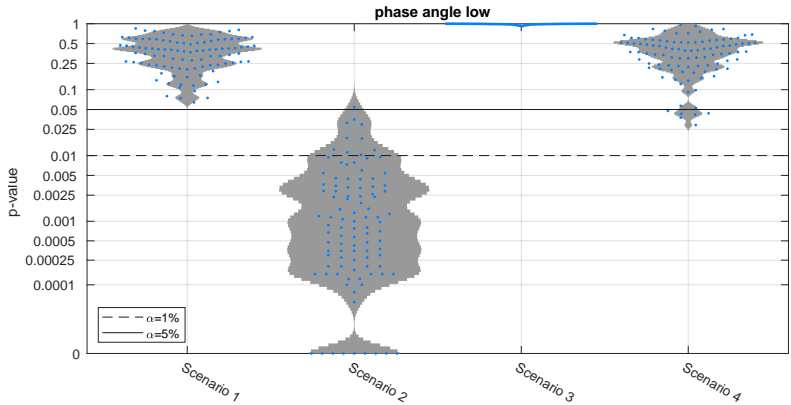
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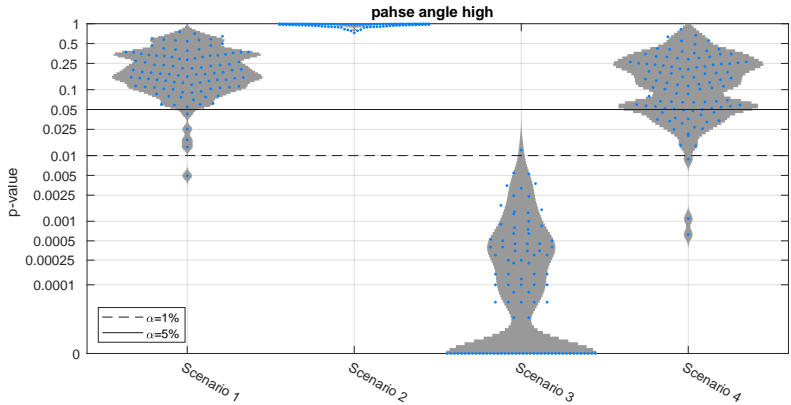
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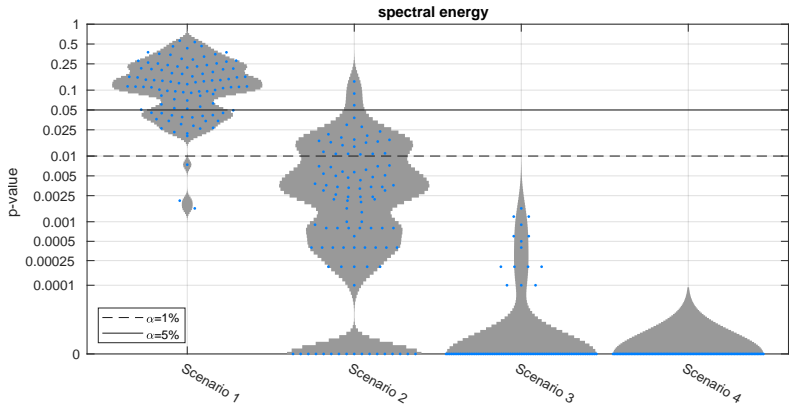
Monte Carlo simulation of all 4 scenarios with sample size $N = 100$. And apply all 3 tests.

TESTING RESULTS



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- Stochastic FIOs for damage detection

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Outlook:

- Surface waves / surface induced waves
- Non-isotropic case

Thank you!



FFG

INTALES